

# Optimization of trusses under uncertain loads.

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#### Optimization of trusses

- Standard minimum compliance truss design.
- Instabilities and the standard multiload model.
- Random Perturbations: Minimizing the expected compliance.
- Numerical examples.
- Random Perturbations: Minimizing the variance.
- Numerical examples.



# **Optimization of trusses**



### Introduction

- Definition.
- Problem: find the best structure able to carry a external nodal force.
- Constraints: mechanical equilibrium, total volume and others ...
- Minimize the compliance.





$$\min_{\lambda,u} \frac{1}{2} f^T u$$
  
s.t.  $K(\lambda)u = f$   
 $\lambda \in \Delta_m$ 

$$\frac{1}{2}f^T u$$
 is called *Compliance*.



#### Mathematical formulation

- $\lambda \in \mathbb{R}^m$ ; *m* number of bars.
- *n* grades of freedom.
- $f \in \mathbb{R}^n$  nodal load vector.
- $u \in \mathbb{R}^n$  nodal displacements.

 $\min_{\lambda,u} \frac{1}{2} f^T u$ s.t.  $K(\lambda)u = f$  $\lambda \in \Delta_m$ 

• 
$$\Delta_m = \{\lambda \in \mathbb{R}^m \mid \lambda \ge 0, \sum_{i=1}^m \lambda_i = 1\}.$$

•  $K(\lambda) \in \mathbb{R}^{n \times n}$ , stiffness matrix.



#### Stiffness Matrix

$$K(\lambda) = \sum_{i=1}^{m} \lambda_i K_i$$

where

$$K_i = b_i b_i^T \in \mathbb{R}^{n \times n}$$

 $K_i$  is dyadic.



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 $K_i$  is dyadic.

$$b_i = \frac{\sqrt{E_i}}{l_i} \gamma_i \in \mathbb{R}^n$$

- $E_i$ : Young modulus.
- $l_i$ : length of bar i.
- $\gamma_i$ : cosines/sines vector.



















- Nodal positions are fixed in the reference configuration.
- We use a mesh full of nodes and bars.





Typically a large number of bar vanish at the optimum.



 $(\mathcal{D})$ 

$$\min_{\lambda \in \mathbb{R}^m, u \in \mathbb{R}^n} rac{1}{2} f^T u$$
  
 $s.t. \ K(\lambda)u = f$   
 $\lambda \in \Delta_m$ 

 $\frac{1}{2}f^T u$  is independent of u satisfying  $K(\lambda)u = f$ .



$$(\mathcal{D}) \quad \min_{\lambda \in \Delta_m} \{ \frac{1}{2} f^T u \mid K(\lambda) u = f \}$$

$$(\mathcal{D}) \quad \min_{\lambda \in \Delta_m} \max_{x \in \mathbb{R}^n} \{ f^T x - \frac{1}{2} x^T K(\lambda) x \}$$

$$(\mathcal{D}) \quad (\text{Minimax Theorem})$$

$$(\mathcal{P}) \quad \min_{x \in \mathbb{R}^n} \max_{1 \le i \le m} \{ \frac{1}{2} x^T K_i x - f^T x \}$$



### Instabilities and the standard multiload model



The design problem (D) may produce unsatisfactory results in respect to mechanical stability (see Ben-Tal and Nemirovsky 1997)



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#### Multiload model

#### **Standard multiload model**

$$\min_{\lambda \in \mathbb{R}^m} \frac{1}{2} \sum_{j=1}^k \alpha_j f^{jT} u^j$$
  
s.t.  $K(\lambda) u^j = f^j, \quad j = 1, \dots, k$   
 $\lambda \in \Delta_m$ 

We minimize a weighted average of the compliances.



#### Multiload model

#### Defining

$$\hat{f} = (\alpha_1 f^{1T}, \dots, \alpha_k f^{kT})^T \in \mathbb{R}^{n(k+1)},$$
$$\hat{K}_i = \operatorname{diag}(\alpha_1 K_i, \dots, \alpha_k K_i) \in \mathbb{R}^{n(k+1) \times n(k+1)},$$
$$\hat{K}(\lambda) = \sum_{i=1}^m \lambda_i \hat{K}_i,$$

Then multiload model can be written as (D). remark:  $\hat{K} \neq b_i b_i^T$ .



# Random Perturbations: Minimizing the expected compliance.



Let  $\xi \in \mathbb{R}^n$  be a perturbation on the load vector f.

 $\Psi(\xi,\lambda) = \begin{cases} \frac{1}{2}(f+\xi)^T x & \text{if } \lambda \in \Delta_m \text{ and } u \in \mathbb{R}^n \text{ such that} \\ K(\lambda)u = f + \xi, \\ +\infty & \text{otherwise} \end{cases}$ 

 $\Psi\colon (\mathbb{R}^n, \mathcal{B}(\mathbb{R}^n)) \to (\mathbb{R} \cup \{+\infty\}, \bar{\mathcal{B}}(\mathbb{R}))$ 

Results to be proper, lower semicontinuous and convex.



For each  $\lambda \in \Delta_m$ 

 $\Psi(\cdot,\lambda): \quad (\mathbb{R}^n,\mathcal{B}(\mathbb{R}^n)) \to (\mathbb{R} \cup \{+\infty\},\bar{\mathcal{B}}(\mathbb{R}))$  $\xi \mapsto \Psi(\xi,\lambda)$ 

#### is measurable.



Minimum expected compliance design problem

 $(\mathcal{D}; \mathbb{P}) \qquad \qquad \min_{\lambda \in \Delta^m} \mathbb{E}_{\xi}[\Psi(\xi, \lambda)]$ 

We assume that  $\xi$  is a random variable corresponding to an uncertain nodal load perturbation

$$\begin{aligned} \xi \colon & (\Omega, \mathcal{A}) & \to & (\mathbb{R}^n, \mathcal{B}(\mathbb{R}^n)) \\ & \omega & \mapsto & \xi(\omega) \end{aligned}$$



1.  $\mathbb{P}$  with finite support  $\text{Sop}(\mathbb{P}) = \{\xi^1, \dots, \xi^k\}.$ 

$$(\mathcal{D}; \mathbb{P}) \qquad \min_{\lambda \in \mathbb{R}^m} \frac{1}{2} \sum_{j=1}^k \alpha_j f^{jT} u^j$$
$$s.t. \ K(\lambda) u^j = f^j, \quad i = 1, \dots, k$$
$$\lambda \in \Delta_m$$

 $(\mathcal{D}; \mathbb{P})$  is the standard multiload model where  $\alpha_j = \mathbb{P}(\xi = \xi^j)$  and  $f^j = f + \xi^j, j = 1, \dots, k$ .



# Continuous case



#### Continuous case

**Theorem 0.1.** Let  $\xi: \Omega \to \mathbb{R}^n$  be a continuous random variable with mean vector  $\mathbb{E}(\xi) = 0$  and Variance–covariance matrix  $\operatorname{Var}(\xi) = PP^T$ , with  $P \in \mathbb{R}^{n \times k}$ . Then the corresponding minimum expected compliance design problem  $(\mathcal{D}; \mathbb{P})$  is given by

$$\mathcal{D}; \mathbb{P}) \quad \min_{\lambda \in \mathbb{R}^m} \underbrace{\frac{1}{2} f^T u}_{\text{mean load}} + \underbrace{\frac{1}{2} \operatorname{Trace}(P^T U)}_{\text{variance}}$$

$$s.t. \ K(\lambda)u = f$$

$$K(\lambda)U = P$$

$$\lambda \in \Delta_m$$



Remark  $p^j$ , j = 1, ..., k, columns of *P* Defining

$$\hat{f} = (f^T, p^{1T}, \dots, p^{kT})^T \in \mathbb{R}^{n(k+1)},$$
$$\hat{K}_i = \operatorname{diag}(K_i, K_i, \dots, K_i) \in \mathbb{R}^{n(k+1) \times n(k+1)},$$
$$\hat{K}(\lambda) = \sum_{i=1}^m \lambda_i \hat{K}_i,$$

Then  $(\mathcal{D}; \mathbb{P})$  may be written as a multiload model.



# Random multidimensional independent perturbation

 $\xi = \sum_{j=1}^{k} \varepsilon_j d^j$ , where  $d^j \in \mathbb{R}^n$ ,  $\mathbb{E}(\varepsilon_j) = 0$  and  $\operatorname{Var}(\varepsilon_j) = \sigma_j^2$ .

$$\mathcal{D}; \mathbb{P}) \qquad \min_{\lambda \in \mathbb{R}^m} \frac{1}{2} f^T u + \frac{1}{2} \sum_{j=1}^r \sigma_j d^{jT} u^j$$
$$s.t. \ K(\lambda) u = f$$
$$K(\lambda) u^j = \sigma_j d^j \quad j = 1, \dots, k$$
$$\lambda \in \Delta_m.$$

Optimal design of trusses. - p. 25/4



# Numerical results



Toy example

#### Toy example, Ben-Tal and Nemirowski 1997





Problem	compl. mean	max compl.	min compl.
Standard single load	∄	$+\infty$	$+\infty$
(a)	0.025	0.053	0.013
(b)	0.023	0.051	0.012



#### Electricity mast

#### Electricity mast, Achtziger et al. 1992





## Electricity mast











#### Dome





### Dome





# Random Perturbations: Minimizing the variance.



### Stochastic model including variance

#### We consider

 $\min_{\lambda \in \mathbb{R}^m} \alpha \mathbb{E}_{\xi} [\Psi(\xi, \lambda)] + \beta \operatorname{Var}[\Psi(\xi, \lambda)].$ 



#### We consider

$$\min_{\lambda \in \mathbb{R}^m} \alpha \mathbb{E}_{\xi} [\Psi(\xi, \lambda)] + \beta \operatorname{Var}[\Psi(\xi, \lambda)]$$

**Theorem 0.2.**  $\xi \sim \mathcal{N}(0, PP^T)$ . Taking for simplicity  $\alpha = 0$  and  $\beta = 1$ .

$$(\mathcal{D}; \mathbb{P}_{\text{var}}) \min_{\lambda \in \mathbb{R}^m} \frac{1}{2} \left( \operatorname{Trace}((P^T U)^2) + 2f^T U U^T f \right)$$
  
s.t.  $K(\lambda)u = f$   
 $K(\lambda)U = P$   
 $\lambda \in \Delta_m$ 

Apparent harder to solve.

Dome 3D - p. 36/4









#### Michel 3D

























### Boxplot





#### **Boxplot**





- Classical model (single load) don't get good results .
- Random model helps to avoid this problem.
- It's equivalent to multiload one, but another interpretations in weight factors holds.
- Continuous Model.
- We have to know the influence of each perturbation.
- Increase the dimension of the problem.
- Highly non linear.



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#### **Boxplot**

